

# » EDM@AMP «

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Plzeň, October 15<sup>th</sup> 2014



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INSTITUT  
PRODUKTIONSANLAGEN UND  
KONSTRUKTIONSTECHNIK

# Agenda

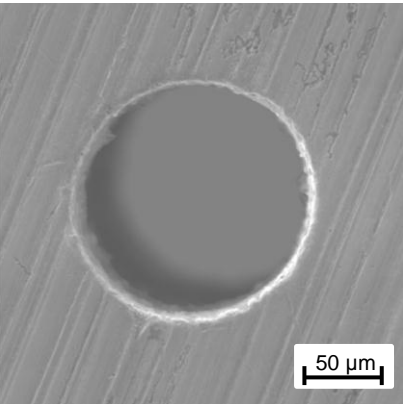
- Dry-EDM Machining of Ceramic Materials
- Process Optimization for Dry-EDM by means of gases
- Our next goals with the Dry-EDM process



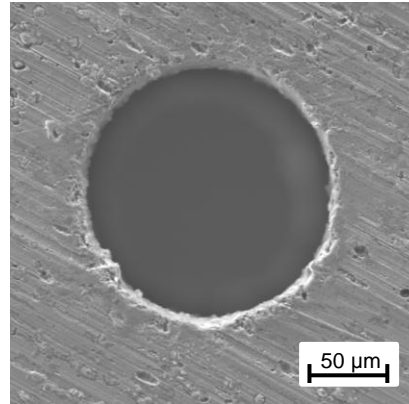


# Dry-EDM Machining of Ceramic Materials

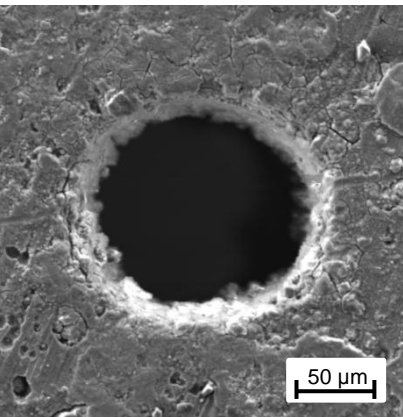
# Dry-EDM Machining of Ceramic Materials



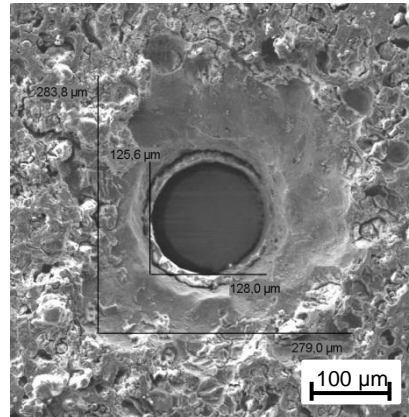
Conductivity of deionized water  $\leq 1,5 \mu\text{S/cm}$



Conductivity of deionized water  $\leq 3 \mu\text{S/cm}$



Conductivity of deionized water  $\leq 7 \mu\text{S/cm}$



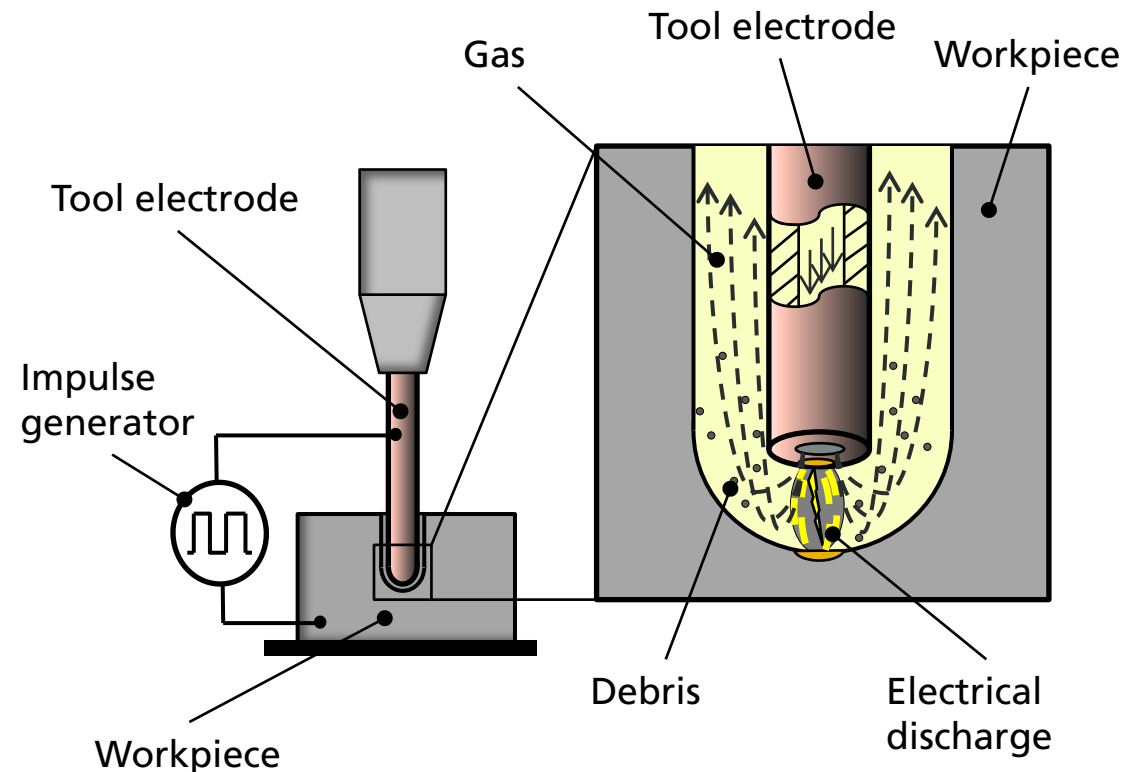
Conductivity of deionized water  $\geq 15 \mu\text{S/cm}$

- Motivation and Challenge:
  - Consequences of contaminated dielectric with debris
    - Fault discharges and short-circuits
    - Reduction of the Material Removal Rate
    - Increase of Tool Electrode Wear
    - Form deviation of the boreholes
- good EDM-machining process is dependent on:
- the dominant flushing conditions in the working gap and
  - the quality of the dielectric fluid

# Dry-EDM Machining of Ceramic Materials

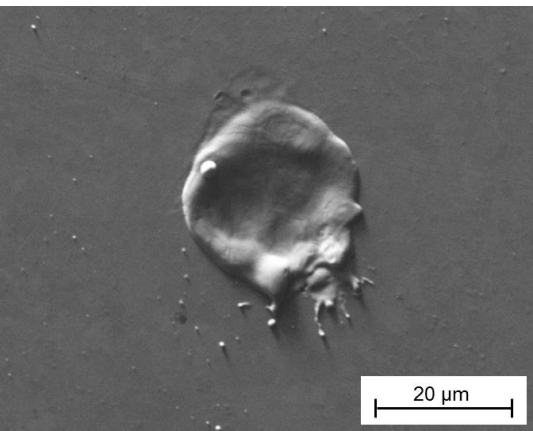
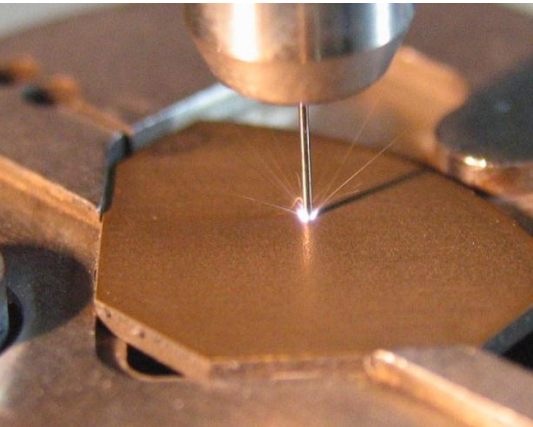
## ■ Objectives and Approach of the presented project

- Replacement of liquid dielectric by gas with the following objectives:
  - Increase the material removal rate compared to the conventional fine drilling
  - Increase of the machining accuracy
  - Reduction of tool electrode wear

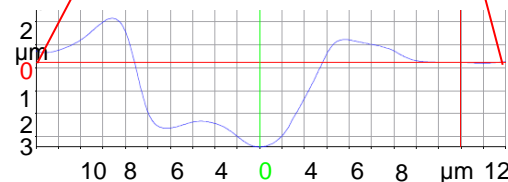
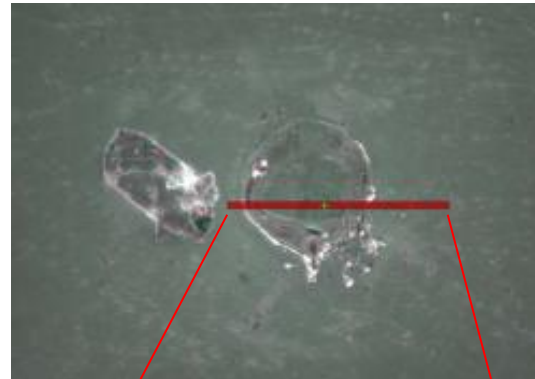




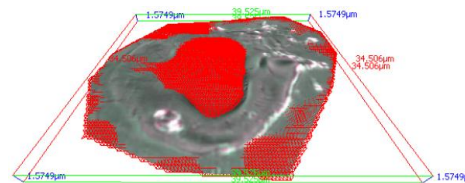
# Dry-EDM Machining of Ceramic Materials



Generation of single relaxation discharge



Metrological evaluation



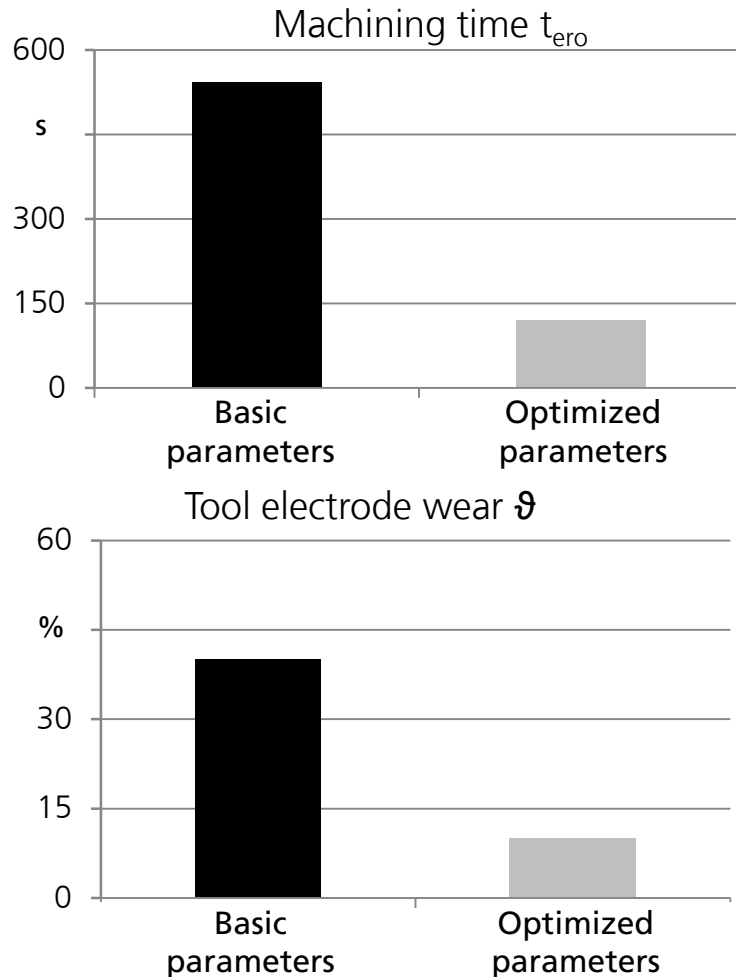
## ■ Solution Approach:

- Targeted single relaxation discharges on workpiece surfaces of the materials TiN, TiB<sub>2</sub>
- Metrological evaluation of the resulting discharge crater
- Development of technologies

## ■ Findings:

- Process behavior of individual parameter settings  
→ derivation of technologies
- Material removal mechanisms of the materials

# Dry-EDM Machining of Ceramic Materials



## Challenges:

- Machining of boreholes in TiN (depth: 1 mm)
- Electrode diameter  $d_{\text{el}} = 300 \mu\text{m}$
- Compressed air as dielectric fluid
- Adjustment of the parameters at the generator through statistical design of experiments

## Result after Process Optimization

- Reduction of the machining time from  $t_{\text{ero}} = 543 \text{ s}$  down to  $t_{\text{ero}} = 120 \text{ s}$  and of the relative tool wear from  $\vartheta = 40 \%$  down to 10 %
- Identification of main and interactive effects

# Dry-EDM Machining of Ceramic Materials

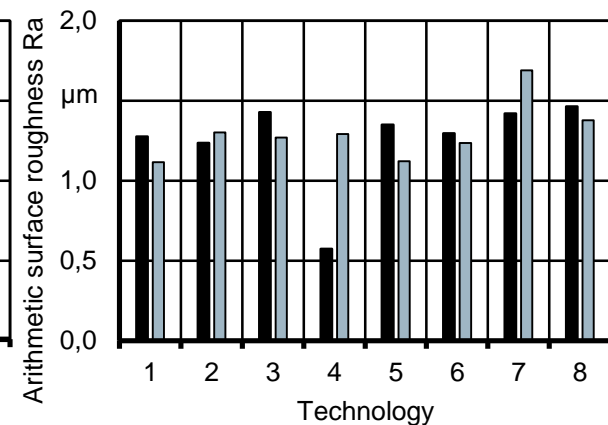
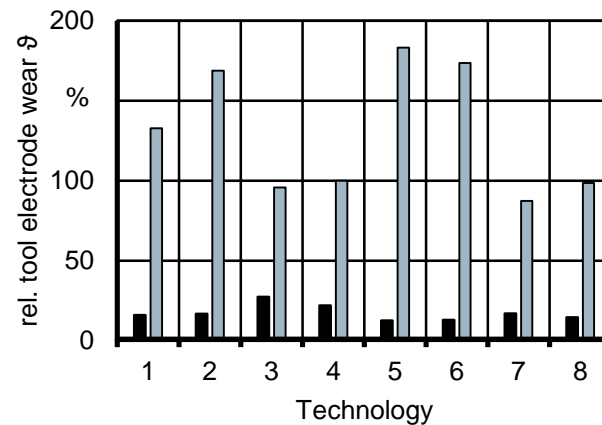
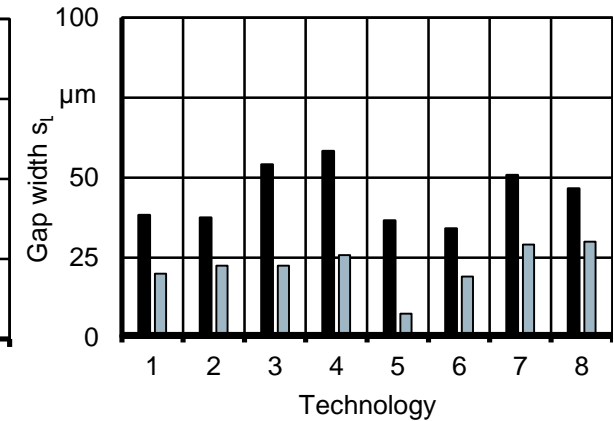
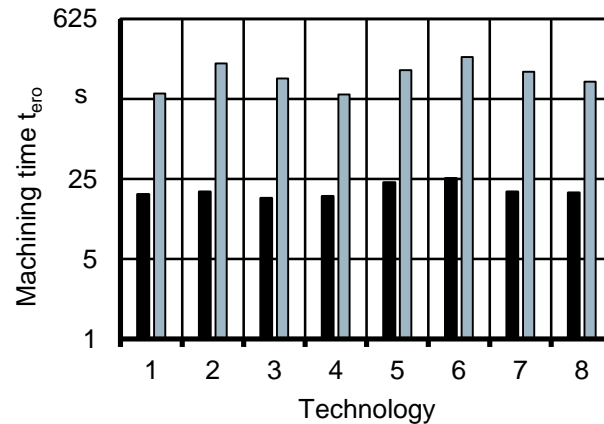
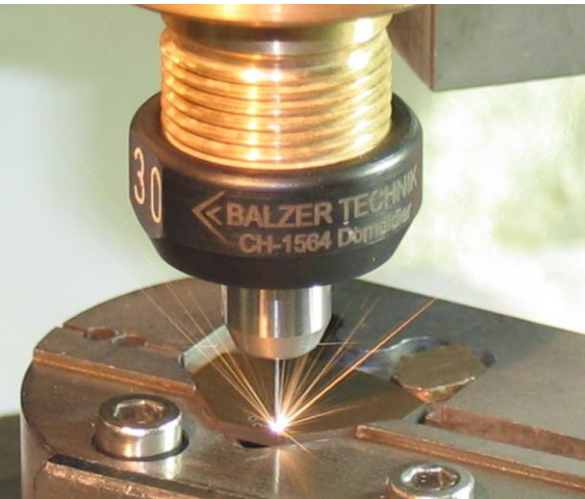
Workpiece materials: ■ TiN  
 ■ TiB<sub>2</sub>

Tool electrode: cemented carbide  $d_{el} = 300 \mu\text{m}$

Through hole: 1 mm

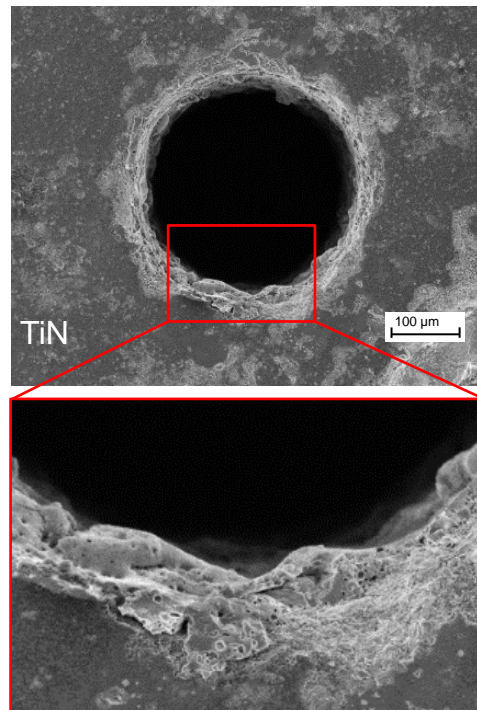
Dielectric fluid: compressed air

Impulse typ: Relaxation discharge

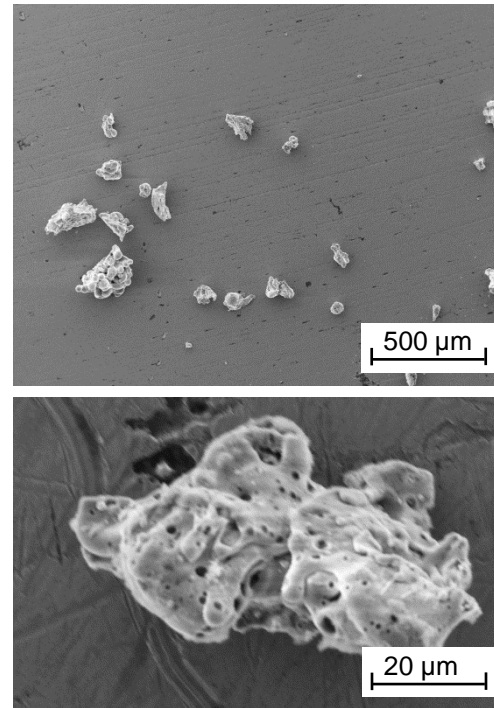




# Dry-EDM Machining of Ceramic Materials



Microhole in TiN

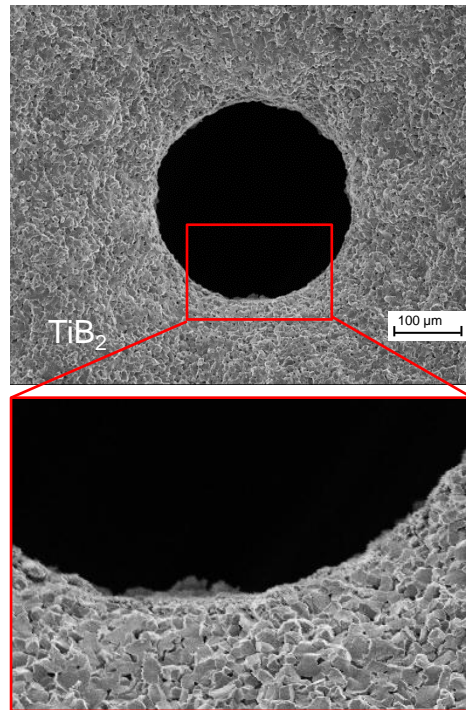


TiN debris of the dry-EDM process

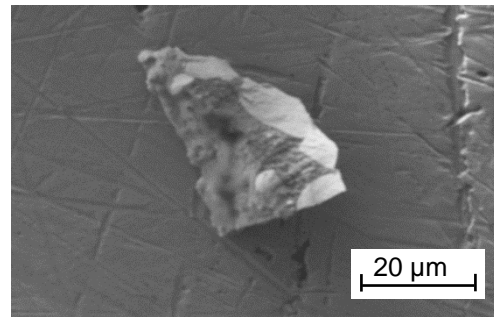
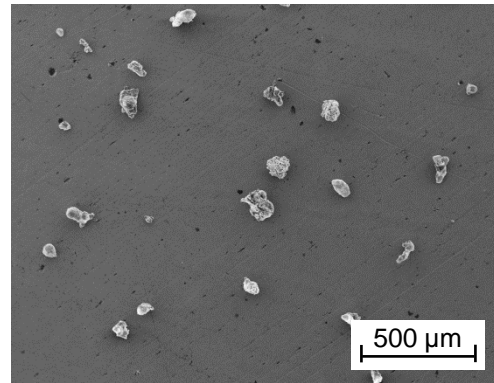
## Results:

- Material removal of TiN is based on the **Melting Effect**
- Less recognition of the Spalling Effect
- Result after process optimization
  - Machining time for 1 mm drilling depth  $t_{\text{ero}} = 16 \text{ s}$
  - Relative tool wear  $\vartheta = 9 \%$
  - Gap width  $s_L = 34 \mu\text{m}$

# Dry-EDM Machining of Ceramic Materials



Microhole in TiB<sub>2</sub>

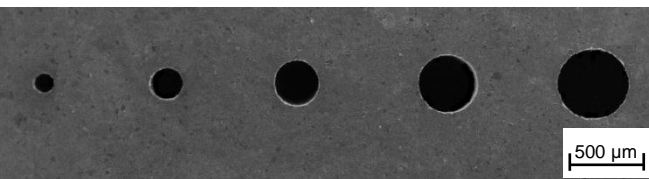
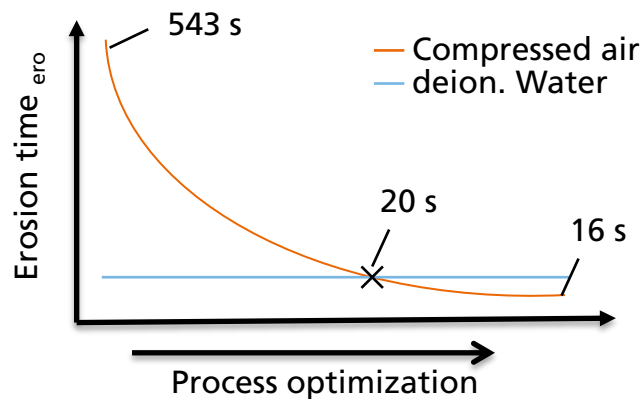


TiB<sub>2</sub> debris of the dry-EDM process

- Material removal of TiB<sub>2</sub> based on the **Spalling Effect**
- No recognition of the Melting Effect
- Result after process optimization
  - Machining time for 1 mm drilling depth  $t_{\text{ero}} = 120 \text{ s}$
  - Relative tool wear  $\vartheta = 183 \%$
  - Gap width  $s_L = 7 \text{ µm}$

# Dry-EDM Machining of Ceramic Materials

Example: 1 mm depth through borehole in TiN



Dry EDM-machined through boreholes in TiN

## Overall Results:

- Development, analysis and application of the dry EDM fine drilling process
- Provision of production technologies for the EDM machining of TiN and TiB<sub>2</sub> with electrode diameters in the range  $80 \mu\text{m} \leq d_{el} \leq 300 \mu\text{m}$

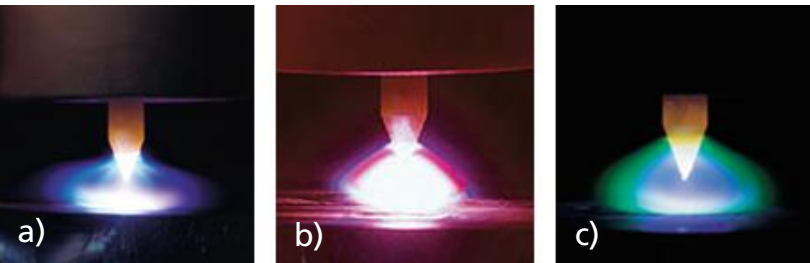
## Innovations:

- No dangerous gases, pollutants or disposal of used oil-based dielectric fluid
- Dielectric tank is no longer required, resulting in a work space without restrictions



# Process Optimization for Dry-EDM by means of gases

# Process Optimization for Dry-EDM by means of gases



a) Argon-, b) VARIGON-, und c) Helium-light arc in TIG-welding



Breidenbach Service + Vertriebs GmbH

„With the TIG method (TIG = Tungsten Inert Gas) the electric arc burns between the non melting tungsten electrode and the workpiece.“ (Linde AG)

## Goals and approach

- Fine-tuning of the process parameters, to the process gases with the aim of:
  - Increasing the material removal rate  
→ Roughing parameter
  - Increase of the exactness and the hole quality by decreasing the electrode wear  
→ Finishing parameter



# Process Optimization for Dry-EDM by means of gases

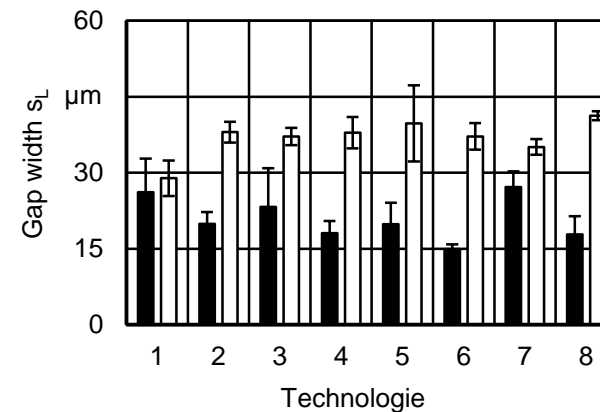
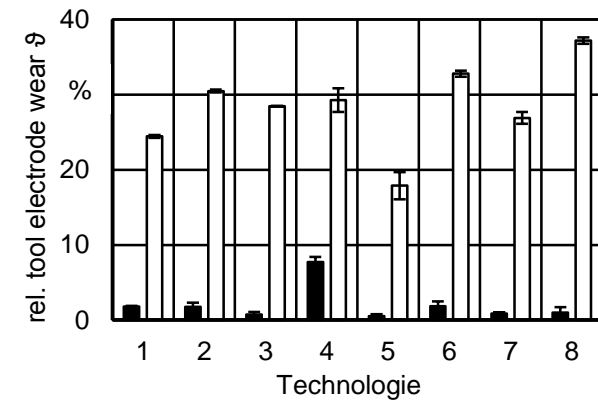
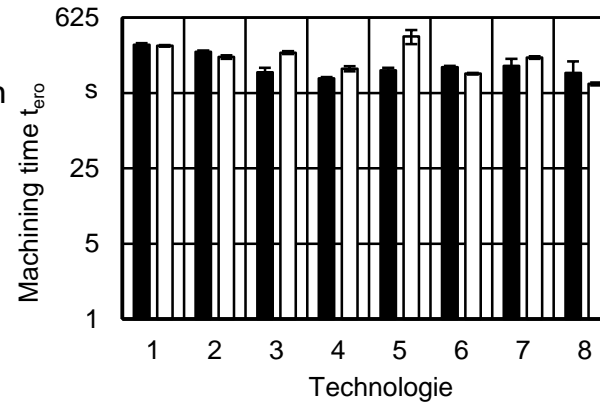
Workpiece material: ■ TiN  
□ TiB<sub>2</sub>

Electrode material: cemented carbide  $d_{el} = 300 \mu\text{m}$

Through hole: 1 mm

Dielectric fluid: argon

Impuls type: relaxation generator





# Process Optimization for Dry-EDM by means of gases

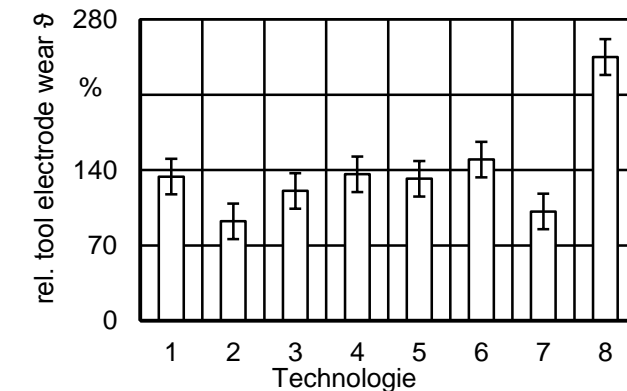
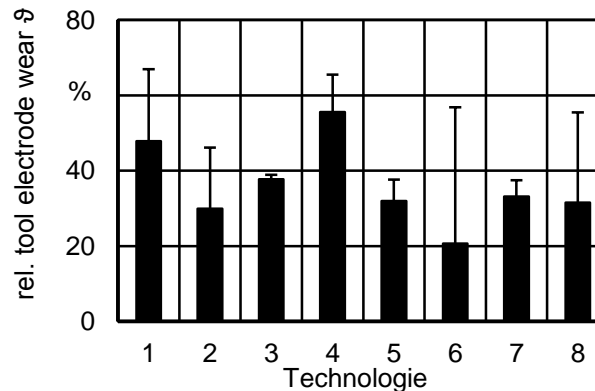
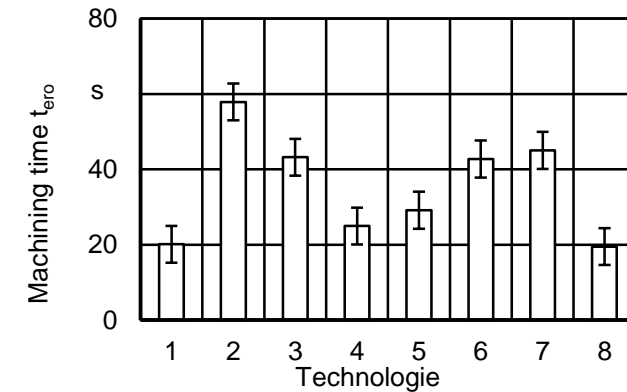
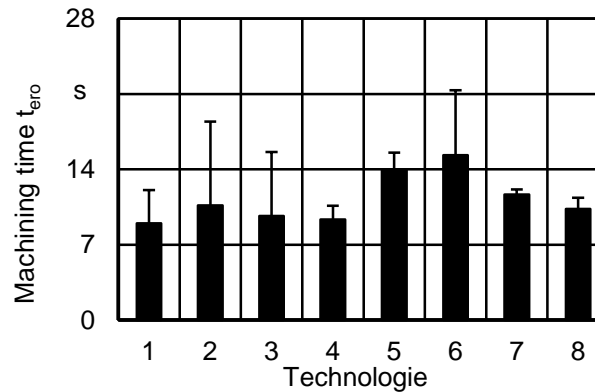
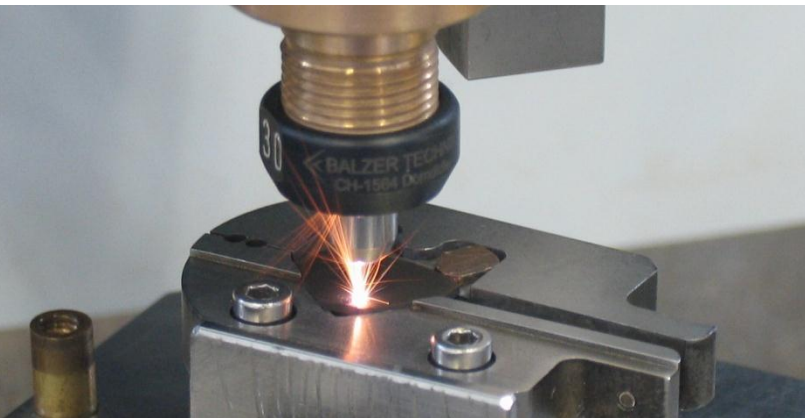
Workpiece material: ■ TiN  
□ TiB<sub>2</sub>

Electrode material: tungsten carbide  
 $d_{el} = 300 \mu\text{m}$

Through hole: 1 mm

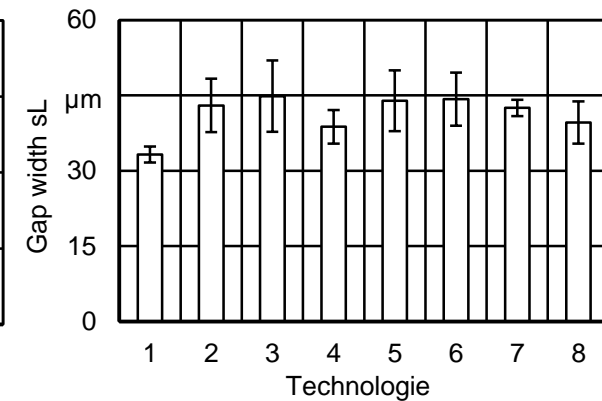
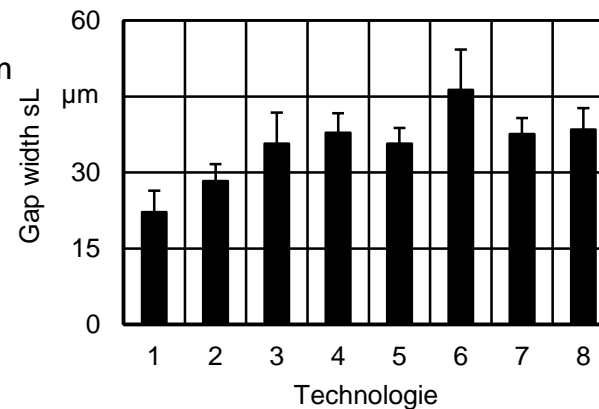
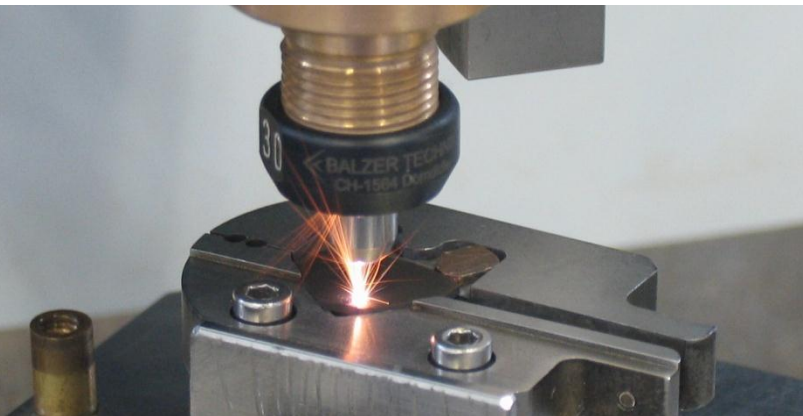
Dielectric fluid: oxygen

Impuls type: relaxation generator



# Process Optimization for Dry-EDM by means of gases

Workpiece material: ■ TiN  
 ■ TiB<sub>2</sub>  
 Electrode material: cemented carbide  $d_{el} = 300 \mu\text{m}$   
 Through hole: 1 mm  
 Dielectric fluid: oxygen  
 Impulse type: relaxation generator

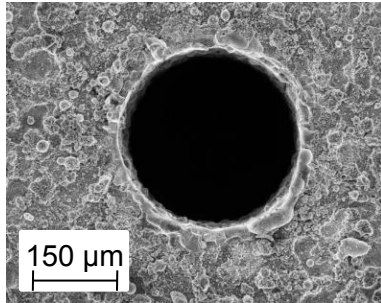


## Following procedure

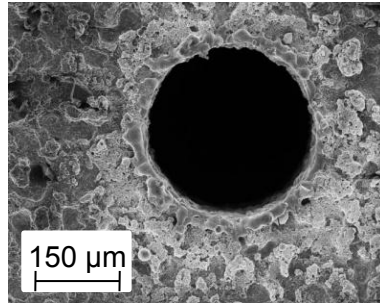
- Systematic parameter optimization, using a specially developed method by Fraunhofer IPK
- Derivation of technologies

# Process Optimization for Dry-EDM by means of gases

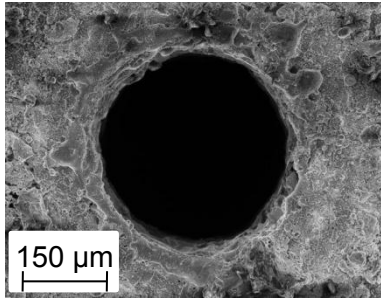
Results of TiN



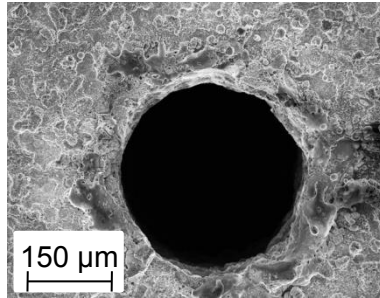
Inlet



Outlet



Inlet



Outlet

## ■ Finishing parameter

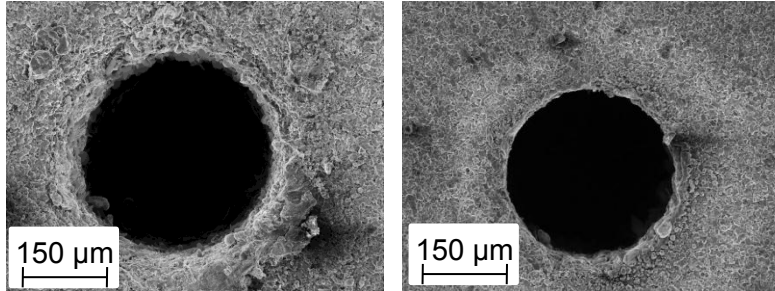
- Machining time  $t_{\text{ero}} = 160 \text{ s}$
- Rel. tool electrode wear  $\vartheta < 0,9 \%$
- Gap width  $s_L = 10 \mu\text{m}$
- Process gas: argon

## ■ Roughing parameter

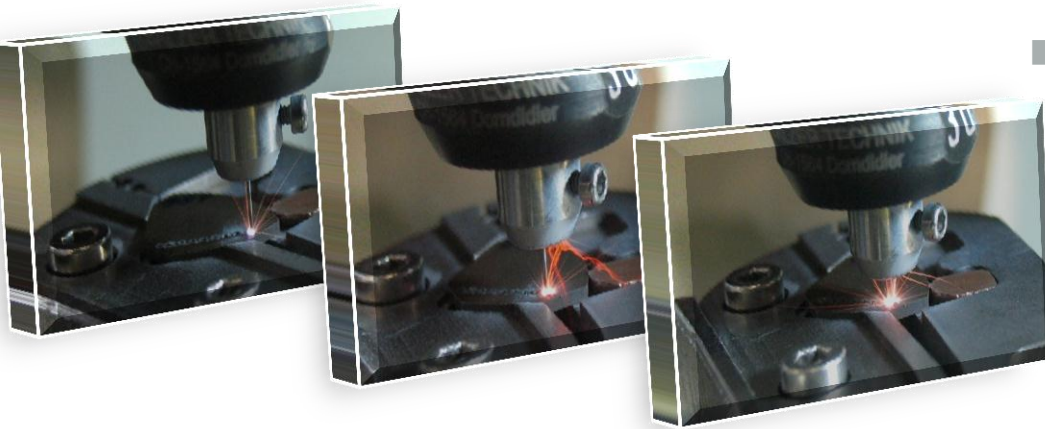
- Machining time  $t_{\text{ero}} = 3,5 \text{ s}$
- Rel. tool electrode wear  $\vartheta = 29 \%$
- Gap width  $s_L = 27 \mu\text{m}$
- Process gas: oxygen

# Process Optimization for Dry-EDM by means of gases

Results of  $\text{TiB}_2$



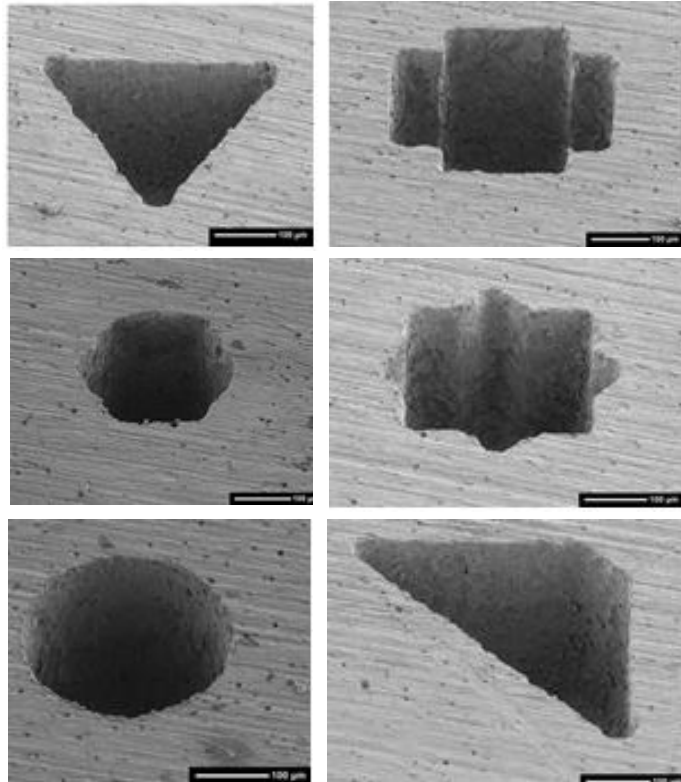
- Finishing parameter
  - Fail (we don't need any finishing!)
- Roughing parameter
  - Machining time  $t_{\text{ero}} = 41 \text{ s}$
  - Rel. tool electrode wear  $\vartheta = 105 \%$
  - Gap width  $s_L = 9 \text{ µm}$
  - Process gas: oxygen





# Our next goals with the Dry-EDM process

# Our next goals with the Dry-EDM process



Complex micro holes manufactured by an  
combined LASER-EDM process

## Development of production technologies for manufacturing complex micro holes

- Using finishing parameters and process gases for manufacturing high precision profile holes
- Using the dry-EDM milling process
- Development of a robot based EDM process
  - High precision
  - High geometrical freedom of the robot, possible because of the dry-EDM process



# Thank you for your attention!



## Contact:

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